

## OPTIMIZATION IN SYMMETRIC ORTHOTROPIC SHELLS

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**Abstract-** The main problems of a modern mechanics, which are contemporary deformed, rigid bodies, are the problems of optimal design of structures. The topic of this work includes questions, which are related to the problems of multilayer structures, those are the problems of optimal design of plates and shells. It is planned to introduce final results based on the structure of Figure 1, and the proposed methods.

**Keywords:** Optimization, Deformation, Orthotropic, Multilayer, Shells.

### I. INTRODUCTION

The shell's deformation state is described mathematically by the system of three differential equations, the form of which is very higher, than one equation form in slabs.

1. The possible reduction of the shell's weight, when the main frequency of shell's own fluctuation is focused, in this paragraph we will observe two cases of the rotation of shells, closed and opened tubular shells [1, 2].

2. Three layered shells, the layers of which is made of homogeneous materials, the middle layer has  $h_0$  constant thickness, but the outer layers, which were arranged symmetrically over the surface of the shell, have changeable  $h_w(\alpha, \beta)$  thickness. [3]

The optimal planning problems of shells for all listed types have the following general definition.

$$M \xrightarrow{h} \min \quad (1)$$

$$\omega = \text{fix} \quad (2)$$

where  $M$  is the weight of shell, and the command parameter  $h$  is defined as function which describes the shell's thickness [4].

$$(0 < h_1 \leq h \leq h_2), \quad h_1, h_2 = \text{const} \quad (3)$$

$$\iint_{\Omega} |\text{grad}h|^2 d\Omega \leq C^2, \quad C = \text{const} \quad (4)$$

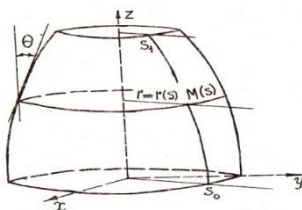


Figure 1. Multilayer structure problem

### II. MATERIALS AND METHODS

$$\begin{aligned} & \frac{d}{dS} \{ rh [ B_{11} (\frac{dU}{dS} + \frac{W}{R_1}) + \frac{B_{12}}{r} (W \cos \theta + U \sin \theta) ] \} + \frac{1}{R_1} \frac{d}{dS} \{ \frac{rh^3}{12} \cdot \\ & \cdot [ B_{11} \frac{d}{dS} (-\frac{dW}{dS} + \frac{U}{R_1}) + B_{12} \frac{\sin \theta}{r} (\frac{dW}{dS} - \frac{U}{R_1}) ] \} + h [ B_{12} (\frac{dU}{dS} + \\ & + \frac{W}{R_1}) + B_{22} \frac{1}{r} (W \cos \theta - U \sin \theta) \sin \theta + \frac{\sin \theta}{R_1} \frac{h^3}{12} [ B_{12} \frac{d}{dS} (-\frac{dW}{dS} + \\ & + \frac{U}{R_1}) + B_{22} \frac{\sin \theta}{r} (\frac{dW}{dS} - \frac{U}{R_1}) ] \} = -r \rho \omega^2 h U = -\omega^2 \psi_3(t) U \end{aligned} \quad (5)$$

$$\begin{aligned} & \frac{d}{dS} \{ \frac{d}{dS} [ \frac{rh^3}{12} ( B_{11} \frac{d}{dS} (-\frac{dW}{dS} + \frac{U}{R_1}) + B_{12} \frac{\sin \theta}{r} \cdot \\ & \cdot (\frac{dW}{dS} + \frac{U}{R_1}) ) ] \} + \frac{h^3 \sin \theta}{12} [ B_{12} \frac{d}{dS} (-\frac{dW}{dS} + \frac{U}{R_1}) + \\ & + B_{22} \frac{\sin \theta}{r} (\frac{dW}{dS} - \frac{U}{R_1}) ] \} - rh \{ \frac{1}{R_1} [ B_{12} (\frac{dU}{dS} + \frac{W}{R_1}) + \\ & + \frac{B_{12}}{r} (W \cos \theta - U \sin \theta) ] \} + \frac{1}{R_2} [ B_{12} (\frac{dU}{dS} + \frac{W}{R_1}) + \\ & + B_{22} \frac{1}{r} (W \cos \theta - U \sin \theta) ] \} = -r \rho \omega^2 h W = -\omega^2 \psi_3(D_3) W \end{aligned}$$

$$\psi_3(D_3) \equiv r \rho h \quad (6)$$

$$D_3 = h(S) \quad (7)$$

where  $S$  is the arc of the line of the shell surface between the point  $M$  and the point  $M_0$  (the beginning of the focused settlement),  $r = r(S)$  is the distance of the point  $M$  from  $OZ$  axis,  $\theta = \theta(S)$  is the angle formed by angle of the point  $M$  with  $OZ$  axis,  $R_1, R_2$  are the main radiuses of the curvature of a rotation surface. For certainty we would assume, that in the shell contour of  $S = S_0$  and  $S = S_1$  are taken place the following marginal conditions [5].

$$W(S) = \frac{dW}{dS} = U(S) = 0, \quad S = S_0, \quad S = S_1 \quad (8)$$

The shells weight fixed with the accuracy of multiplier is given with the following functional way [6].

$$J = \int_{S_0}^S r h dS \quad (9)$$

III. RESULTS AND DISCUSSION

Let's give  $\delta h$  increase to the functional  $h$ , in that case (5) system of equations will be written of this enhancements and will receive as the following [9, 10].

$$\begin{aligned} & \frac{d}{dS} \{ rh + \delta h [ B_{11} (\frac{dU + \delta U}{dS} + \frac{W + \delta W}{R_1}) + \frac{B_{12}}{r} (W + \delta W \cos \theta + \\ & U + \delta U \sin \theta) ] \} + \frac{1}{R_1} \frac{d}{dS} \{ \frac{rh + \delta h^3}{12} [ B_{11} \frac{d}{dS} (-\frac{dW + \delta W}{dS} + \\ & \frac{U + \delta U}{R_1}) + B_{12} \frac{\sin \theta}{r} (\frac{dW + \delta W}{dS} - \frac{U + \delta U}{R_1}) ] \} + h + \quad (10) \\ & + \delta h [ B_{12} (\frac{dU + \delta U}{dS} + \frac{W + \delta W}{R_1}) + B_{22} \frac{1}{r} (W + \delta W \cos \theta - U + \\ & + \delta U \sin \theta) ] + \sin \theta + \frac{\sin \theta}{R_1} \frac{h + \delta h^3}{12} [ B_{12} \frac{d}{dS} (-\frac{dW + \delta W}{dS} + \\ & + \frac{U + \delta U}{R_1}) + B_{22} \frac{\sin \theta}{r} (\frac{dW + \delta W}{dS} - \frac{U + \delta U}{R_1}) ] + r \rho \omega^2 h + \\ & + \delta h U + \delta U = 0 \end{aligned}$$

$$\begin{aligned} & \frac{d}{dS} \{ \frac{d}{dS} [ \frac{rh + \delta h^3}{12} ( B_{11} \frac{d}{dS} (-\frac{dW + \delta W}{dS} + \frac{U + \delta U}{R_1}) + \\ & + B_{12} \frac{\sin \theta}{r} (\frac{dW + \delta W}{dS} + \frac{U + \delta U}{R_1}) ) ] \} + \frac{h + \delta h^3 \sin \theta}{12} \cdot \\ & \cdot [ B_{12} \frac{d}{dS} (-\frac{dW + \delta W}{dS} + \frac{U + \delta U}{R_1}) + B_{22} \frac{\sin \theta}{r} \cdot \quad (11) \\ & \cdot (\frac{dW + \delta W}{dS} - \frac{U + \delta U}{R_1}) ] \} - rh + \delta h \{ \frac{1}{R_1} [ B_{12} (\frac{dU + \delta U}{dS} + \\ & + \frac{W + \delta W}{R_1}) + \frac{B_{12}}{r} (W + \delta W \cos \theta - U + \delta U \sin \theta) ] + \\ & + \frac{1}{R_2} [ B_{12} (\frac{dU + \delta U}{dS} + \frac{W + \delta W}{R_1}) + B_{22} \frac{1}{r} (W + \delta W \cos \theta - \\ & - U + \delta U \sin \theta) ] \} + r \rho \omega^2 h + \delta h W + \delta W = 0 \end{aligned}$$

Taking into consideration (5) the equations and ignoring  $\delta h$ ,  $\delta U$ ,  $\delta W$  enhancement of the small quantities of the second order we will get [7, 8]:

$$\begin{aligned} & \frac{d}{dS} \{ r [ B_{11} h \frac{d\delta U}{dS} + B_{11} \delta h \frac{dU}{dS} + B_{11} h \frac{\delta W}{R_1} + B_{11} \delta h \frac{W}{R_1} + \frac{B_{12}}{r} h \cdot \\ & \cdot \delta W \cos \theta + \frac{B_{12}}{r} \delta h W \cos \theta + \frac{B_{12}}{r} h \delta U \sin \theta + \frac{B_{12}}{r} \delta h U \sin \theta ] \} + \\ & + \frac{1}{R_1} \frac{d}{dS} \{ \frac{r}{12} [ -B_{11} \frac{d}{dS} h^3 \frac{d\delta W}{dS} - B_{11} \frac{d}{dS} 3h^2 \delta h \frac{dW}{dS} + \\ & + B_{11} \frac{d}{dS} h^3 \frac{\delta U}{R_1} + B_{11} \frac{d}{dS} 3h^2 \delta h \frac{U}{R_1} + B_{12} \frac{\sin \theta}{r} \frac{d}{dS} h^3 \frac{d\delta W}{dS} + \\ & + B_{12} \frac{\sin \theta}{r} \frac{d}{dS} 3h^2 \delta h \frac{dW}{dS} - B_{12} \frac{\sin \theta}{r} \frac{d}{dS} h^3 \frac{\delta U}{R_1} - \end{aligned}$$

$$\begin{aligned} & - B_{12} \frac{\sin \theta}{r} \frac{d}{dS} 3h^2 \delta h \frac{U}{R_1} ] \} + [ B_{12} h \frac{d\delta U}{dS} + B_{12} \delta h \frac{dU}{dS} + \\ & + B_{12} h \frac{\delta W}{R_1} + B_{12} \delta h \frac{W}{R_1} + B_{22} \frac{1}{r} h \delta W \cos \theta + B_{22} \frac{1}{r} \delta h W \cos \theta - \\ & - B_{22} \frac{1}{r} h \delta U \sin \theta - B_{22} \frac{1}{r} \delta h U \sin \theta ] \sin \theta + \frac{\sin \theta}{R_1} \frac{1}{12} \cdot \\ & \cdot [ -B_{12} \frac{d}{dS} h^3 \frac{d\delta W}{dS} - B_{12} \frac{d}{dS} 3h^2 \delta h \frac{dW}{dS} + B_{12} \frac{d}{dS} h^3 \frac{\delta U}{R_1} + \\ & + B_{12} \frac{d}{dS} 3h^2 \delta h \frac{U}{R_1} + B_{22} \frac{\sin \theta}{r} h^3 \frac{d\delta W}{dS} + \quad (12) \\ & + B_{22} \frac{\sin \theta}{r} 3h^2 \delta h \frac{dW}{dS} - B_{22} \frac{\sin \theta}{r} h^3 \frac{\delta U}{R_1} - \\ & - B_{22} \frac{\sin \theta}{r} 3h^2 \delta h \frac{U}{R_1} ] + r \rho \omega^2 h \delta U + r \rho \omega^2 \delta h U = 0 \end{aligned}$$

$$\begin{aligned} & \frac{d}{dS} \{ \frac{d}{dS} [ \frac{r}{12} ( -B_{11} h^3 \frac{d\delta W}{dS} - B_{11} 3h^2 \delta h \frac{dW}{dS} + B_{11} h^3 \frac{\delta U}{R_1} + \\ & + B_{11} 3h^2 \delta h \frac{U}{R_1} + B_{12} \frac{\sin \theta}{r} h^2 \frac{d\delta W}{dS} + B_{12} \frac{\sin \theta}{r} 3h^2 \delta h \frac{dW}{dS} + \\ & + B_{12} \frac{\sin \theta}{r} h^3 \frac{\delta U}{R_1} + B_{12} \frac{\sin \theta}{r} 3h^2 \delta h \frac{U}{R_1} ) ] \} + \frac{\sin \theta}{12} [ -B_{12} \frac{d}{dS} \cdot \\ & \cdot h^3 \frac{d\delta W}{dS} - B_{12} \frac{d}{dS} 3h^2 \delta h \frac{dW}{dS} + B_{12} \frac{d}{dS} h^3 \frac{\delta U}{R_1} + B_{12} \frac{d}{dS} 3h^2 \cdot \\ & \cdot \delta h \frac{U}{R_1} + B_{22} \frac{\sin \theta}{r} h^3 \frac{d\delta W}{dS} + B_{22} \frac{\sin \theta}{r} 3h^2 \delta h \frac{dW}{dS} - \quad (13) \\ & - B_{22} \frac{\sin \theta}{r} h^3 \frac{\delta U}{R_1} - B_{22} \frac{\sin \theta}{r} 3h^2 \delta h \frac{U}{R_1} ] \} - r \{ \frac{1}{R_1} [ B_{12} h \frac{d\delta U}{dS} + \\ & + B_{12} \delta h \frac{dU}{dS} + B_{12} h \frac{\delta W}{R_1} + B_{12} \delta h \frac{W}{R_1} + B_{12} \frac{1}{r} h \delta W \cos \theta + \\ & + B_{12} \frac{1}{r} \delta h W \cos \theta - B_{12} \frac{1}{r} h \delta U \sin \theta - B_{12} \frac{1}{r} \delta h U \sin \theta ] + \\ & + \frac{1}{R_2} [ B_{12} h \frac{d\delta U}{dS} + B_{12} \delta h \frac{dU}{dS} + B_{12} h \frac{\delta W}{R_1} + B_{12} \delta h \frac{W}{R_1} + \\ & + B_{22} \frac{1}{r} h \delta W \cos \theta + B_{22} \frac{1}{r} \delta h W \cos \theta - B_{22} \frac{1}{r} h \delta U \sin \theta - \\ & - B_{22} \frac{1}{r} \delta h U \sin \theta ] \} + r \rho \omega^2 h \delta W + r \rho \omega^2 \delta h W = 0 \end{aligned}$$

The Functional purpose will also receive increases

$$\delta J = \int_{S_0}^S r \delta h dS \quad (14)$$

Let's multiply the first and the second left parts of the systems Equation (13) accordingly with the  $U_1$ ,  $W_1$  functions. The amount of obtained expressions integrate to  $S_0 - S$ , than to add Equation (14) [9, 10].

$$\begin{aligned}
 & \left[ \frac{d}{ds} \left\{ r[B_{11}h \frac{d\delta U}{ds} + B_{11}\delta h \frac{dU}{ds} + B_{11}h \frac{\delta W}{R_1} + B_{11}\delta h \frac{W}{R_1} + \right. \right. \\
 & \left. \left. + \frac{B_{12}}{r} h\delta W \cos \theta + \frac{B_{12}}{r} \delta h W \cos \theta + \frac{B_{12}}{r} h\delta U \sin \theta + \right. \right. \\
 & \left. \left. + \frac{B_{12}}{r} \delta h U \sin \theta \right\} + \frac{1}{R_1} \frac{d}{ds} \left\{ \frac{r}{12} [-B_{11} \frac{d}{ds} h^3 \frac{d\delta W}{ds} - \right. \right. \\
 & \left. \left. -B_{11} \frac{d}{ds} 3h^2 \delta h \frac{dW}{ds} + B_{11} \frac{d}{ds} h^3 \frac{\delta U}{R_1} + B_{11} \frac{d}{ds} 3h^2 \delta h \frac{U}{R_1} + \right. \right. \\
 & \left. \left. + B_{12} \frac{\sin \theta}{r} \frac{d}{ds} h^3 \frac{d\delta W}{ds} + B_{12} \frac{\sin \theta}{r} \frac{d}{ds} 3h^2 \delta h \frac{dW}{ds} - \right. \right. \\
 & \left. \left. -B_{12} \frac{\sin \theta}{r} \frac{d}{ds} h^3 \frac{\delta U}{R_1} - B_{12} \frac{\sin \theta}{r} \frac{d}{ds} 3h^2 \delta h \frac{U}{R_1} \right\} \right] + \\
 & \left[ B_{12} h \frac{d\delta U}{ds} + B_{12} \delta h \frac{dU}{ds} + B_{12} h \frac{\delta W}{R_1} + B_{12} \delta h \frac{W}{R_1} + \right. \\
 & \left. + B_{22} \frac{1}{r} h\delta W \cos \theta + B_{22} \frac{1}{r} \delta h W \cos \theta - B_{22} \frac{1}{r} h\delta U \sin \theta - \right. \\
 & \left. - B_{22} \frac{1}{r} \delta h U \sin \theta \right] \sin \theta + \frac{\sin \theta}{R_1} \frac{1}{12} [-B_{12} \frac{d}{ds} h^3 \frac{d\delta W}{ds} - \\
 & -B_{12} \frac{d}{ds} 3h^2 \delta h \frac{dW}{ds} + B_{12} \frac{d}{ds} h^3 \frac{\delta U}{R_1} + B_{12} \frac{d}{ds} 3h^2 \delta h \frac{U}{R_1} + \\
 & + B_{22} \frac{\sin \theta}{r} h^3 \frac{d\delta W}{ds} + B_{22} \sin 3h^2 \delta h \frac{dW}{ds} - B_{22} \frac{\sin \theta}{r} h^3 \frac{\delta U}{R_1} - \\
 & B_{22} \frac{\sin \theta}{r} 3h^2 \delta h \frac{U}{R_1}] + r\rho\omega^2 h\delta U + r\rho\omega^2 \delta h U U_1 + \quad (15) \\
 & \left[ \frac{d}{ds} \left\{ \frac{d}{ds} \left[ \frac{r}{12} (-B_{11} \frac{d}{ds} h^3 \frac{d\delta W}{ds} - B_{11} \frac{d}{ds} 3h^2 \delta h \frac{dW}{ds} + \right. \right. \right. \\
 & \left. \left. + B_{11} \frac{d}{ds} h^3 \frac{\delta U}{R_1} + B_{11} \frac{d}{ds} 3h^2 \delta h \frac{U}{R_1} + B_{12} \frac{\sin \theta}{r} h^2 \frac{d\delta W}{ds} + \right. \right. \\
 & \left. \left. + B_{12} \frac{\sin \theta}{r} 3h^2 \delta h \frac{dW}{ds} + B_{12} \frac{\sin \theta}{r} h^3 \frac{\delta U}{R_1} + B_{12} \frac{\sin \theta}{r} 3h^2 \delta h \frac{U}{R_1} \right) \right] + \\
 & \left. + \frac{\sin \theta}{12} [-B_{12} \frac{d}{ds} h^3 \frac{d\delta W}{ds} - B_{12} \frac{d}{ds} 3h^2 \delta h \frac{dW}{ds} + B_{12} \frac{d}{ds} h^3 \frac{\delta U}{R_1} + \right. \\
 & \left. + B_{12} \frac{d}{ds} 3h^2 \delta h \frac{U}{R_1} + B_{22} \frac{\sin \theta}{r} h^3 \frac{d\delta W}{ds} + B_{22} \frac{\sin \theta}{r} 3h^2 \delta h \frac{dW}{ds} - \right. \\
 & \left. - B_{22} \frac{\sin \theta}{r} h^3 \frac{\delta U}{R_1} - B_{22} \frac{\sin \theta}{r} 3h^2 \delta h \frac{U}{R_1} \right] - r \left\{ \frac{1}{R_1} [B_{12} h \frac{d\delta U}{ds} + \right. \\
 & \left. + B_{12} \delta h \frac{dU}{ds} + B_{12} h \frac{\delta W}{R_1} + B_{12} \delta h \frac{W}{R_1} + B_{12} \frac{1}{r} h\delta W \cos \theta + \right. \\
 & \left. + B_{12} \frac{1}{r} \delta h W \cos \theta - B_{12} \frac{1}{r} h\delta U \sin \theta - B_{12} \frac{1}{r} \delta h U \sin \theta \right] + \\
 & \left. + \frac{1}{R_2} [B_{12} h \frac{d\delta U}{ds} + B_{12} \delta h \frac{dU}{ds} + B_{12} h \frac{\delta W}{R_1} + B_{12} \delta h \frac{W}{R_1} + \right. \\
 & \left. + B_{22} \frac{1}{r} h\delta W \cos \theta + B_{22} \frac{1}{r} \delta h W \cos \theta - B_{22} \frac{1}{r} h\delta U \sin \theta - \right. \\
 & \left. - B_{22} \frac{1}{r} \delta h U \sin \theta \right] + r\rho\omega^2 h\delta W + r\rho\omega^2 \delta h W [W_1 + \delta h] ds
 \end{aligned}$$

In the integrate excretion we get let's do grouping by  $\delta h$ ,  $\delta U$ ,  $\delta W$  enhancements. So (15) this integrate will have the following outlook [11, 12].

$$\begin{aligned}
 & \int_{S_0}^S \left[ \left\{ r[B_{11}\delta U \frac{d}{ds} h \frac{dU_1}{ds} - B_{11}\delta h \frac{dU_1}{ds} \frac{dU}{ds} - \frac{B_{11}}{R_1} h \frac{dU_1}{ds} \delta W - \right. \right. \\
 & \left. \left. - \frac{B_{11}}{R_1} \delta h \frac{dU_1}{ds} W + \frac{B_{12}}{r} h \frac{dU_1}{ds} \delta W \cos \theta - \frac{B_{12}}{r} \delta h \frac{dU_1}{ds} W \cos \theta - \right. \right. \\
 & \left. \left. - \frac{B_{12}}{r} h \frac{dU_1}{ds} \delta U \sin \theta - \frac{B_{12}}{r} \delta h \frac{dU_1}{ds} U \sin \theta \right\} + \frac{1}{R_1} \left\{ \frac{r}{12} \right. \right. \\
 & \left. \left. [-B_{11}\delta W \frac{d^2}{ds^2} h^3 \frac{dU_1}{ds} + 3B_{11}h^2 \delta h \frac{d^2 W}{ds^2} \frac{dU_1}{ds} + \frac{B_{11}}{R_1} \frac{d}{ds} h^3 \frac{dU_1}{ds} \right. \right. \\
 & \left. \left. \cdot \delta U + \frac{3B_{11}}{R_1} \frac{d}{ds} h^2 \delta h \frac{dU_1}{ds} U + B_{12} \frac{\sin \theta}{r} \frac{d}{ds} h^3 \frac{dU_1}{ds} \delta W - \right. \right. \\
 & \left. \left. - B_{12} \frac{\sin \theta}{r} \frac{d}{ds} 3h^2 \delta h \frac{dU_1}{ds} W - \frac{B_{12}}{R_1} \frac{\sin \theta}{r} \frac{d}{ds} h^3 \frac{dU_1}{ds} \delta U - \right. \right. \\
 & \left. \left. - \frac{B_{12}}{R_1} \frac{\sin \theta}{r} \frac{d}{ds} 3h^2 \delta h \frac{dU_1}{ds} U \right] + [B_{12}\delta U \frac{dhU_1}{ds} - B_{12}\delta h \frac{dU}{ds} U_1 - \right. \\
 & \left. - \frac{B_{12}}{R_1} h\delta W U_1 - \frac{B_{12}}{R_1} \delta h W U_1 - B_{22} \frac{1}{r} h\delta W U_1 \cos \theta + \right. \\
 & \left. + B_{22} \frac{1}{r} \delta h W U_1 \cos \theta + B_{22} \frac{1}{r} h\delta U U_1 \sin \theta + B_{22} \frac{1}{r} \delta h U U_1 \sin \theta \right] \cdot \\
 & \left. \sin \theta + \frac{\sin \theta}{R_1} \frac{1}{12} [-B_{12}\delta W \frac{d^2}{ds^2} h^3 \frac{dU_1}{ds} + +3B_{12}h^2 \delta h \frac{d^2 W}{ds^2} \right. \\
 & \left. \cdot \frac{dU_1}{ds} - \frac{B_{12}}{R_1} \frac{d}{ds} h^3 \frac{dU_1}{ds} \delta U - \frac{3B_{12}}{R_1} \frac{d}{ds} h^2 \delta h \frac{dU_1}{ds} U + B_{22} \frac{\sin \theta}{r} \right. \\
 & \left. \cdot h^3 \frac{dU_1}{ds} \delta W - B_{22} \frac{\sin \theta}{r} 3h^2 \delta h \frac{dU_1}{ds} W + \frac{B_{22}}{R_1} \frac{\sin \theta}{r} h^3 \delta U U_1 + \right. \\
 & \left. + \frac{B_{22}}{R_1} \frac{\sin \theta}{r} 3h^2 \delta h U U_1 \right] + r\rho\omega^2 h\delta U U_1 + r\rho\omega^2 \delta h U U_1 + \\
 & \left. + \frac{r}{12} (B_{11}\delta W \frac{d^3}{ds^3} h^3 \frac{dW_1}{ds} - B_{11} \frac{d^3}{ds^3} 3h^2 \delta h \frac{dW_1}{ds} \frac{dW}{ds} - \right. \\
 & \left. - \frac{B_{11}}{R_1} \frac{d^3}{ds^3} h^3 \frac{dW_1}{ds} \delta U - \frac{B_{11}}{R_1} \frac{d^3}{ds^3} 3h^2 \delta h \frac{dW_1}{ds} U + \right. \quad (16) \\
 & \left. + B_{12}\delta W \frac{\sin \theta}{r} \frac{d^2}{ds^2} h^2 \frac{dW_1}{ds} - B_{12} \frac{\sin \theta}{r} \frac{d^2}{ds^2} 3h^2 \delta h \frac{dW_1}{ds} \frac{dW}{ds} - \right. \\
 & \left. - \frac{B_{12}}{R_1} \frac{\sin \theta}{r} \frac{d^2}{ds^2} h^3 \delta U W_1 - B_{12} \frac{\sin \theta}{r} \frac{d^2}{ds^2} 3h^2 \delta h U W_1 \right) + \\
 & \left. + \frac{\sin \theta}{12} [-B_{12}\delta W \frac{d^3}{ds^3} h^3 \frac{dW_1}{ds} + B_{12} \frac{d^2}{ds^2} 3h^2 \delta h \frac{dW_1}{ds} \frac{dW}{ds} + \right. \\
 & \left. + \frac{B_{12}}{R_1} \frac{d^2}{ds^2} h^3 \frac{dW_1}{ds} \delta U + \frac{B_{12}}{R_1} \frac{d^2}{ds^2} 3h^2 \delta h \frac{dW_1}{ds} U + \right. \\
 & \left. + B_{22} \frac{\sin \theta}{r} \frac{d^2}{ds^2} h^3 \frac{dW_1}{ds} \delta W - B_{22} \frac{\sin \theta}{r} \frac{d^2}{ds^2} 3h^2 \delta h \frac{dW_1}{ds} \frac{dW}{ds} - \right. \\
 & \left. - \frac{B_{22}}{R_1} \frac{\sin \theta}{r} \frac{d^2}{ds^2} h^3 W_1 \delta U - \frac{B_{22}}{R_1} \frac{\sin \theta}{r} \frac{d^2}{ds^2} 3h^2 \delta h W_1 U \right] - \\
 & \left. - r \left\{ \frac{1}{R_1} [B_{12} \frac{d}{ds} h \frac{dW_1}{ds} \delta U - B_{12} \delta h \frac{dW_1}{ds} \frac{dU}{ds} - \frac{B_{12}}{R_1} h \frac{dW_1}{ds} \delta W - \right. \right. \\
 & \left. \left. - \frac{B_{12}}{R_1} \delta h \frac{dW_1}{ds} W - B_{12} \frac{1}{r} h \frac{dW_1}{ds} \delta W \cos \theta + B_{12} \frac{1}{r} \delta h \frac{dW_1}{ds} \right. \right.
 \end{aligned}$$

$$\begin{aligned}
 & W \cos \theta + B_{12} \frac{1}{r} h \frac{dW_1}{dS} \delta U \sin \theta + B_{12} \frac{1}{r} \delta h \frac{dW_1}{dS} U \sin \theta + \\
 & + \frac{1}{R_2} [B_{12} \frac{d}{dS} h \frac{dW_1}{dS} \delta U - B_{12} \delta h \frac{dW_1}{dS} \frac{dU}{dS} - \frac{B_{12}}{R_1} h \frac{\delta W_1}{dS} \delta W - \\
 & - \frac{B_{12}}{R_1} \delta h \frac{dW_1}{dS} W + B_{22} \frac{1}{r} h \frac{dW_1}{dS} \delta W \cos \theta - B_{22} \frac{1}{r} \delta h \frac{dW_1}{dS} \cdot \\
 & W \cos \theta + B_{22} \frac{1}{r} h \frac{dW_1}{dS} \delta U \sin \theta + + B_{22} \frac{1}{r} \delta h \frac{dW_1}{dS} U \sin \theta] + \\
 & + r \rho \omega^{-2} h \delta W W_1 + r \rho \omega^{-2} \delta h W W_1] dS
 \end{aligned}$$

In (16) integrate expressions let's do grouping by  $\delta h, \delta U, \delta W, \delta V$  enhancement, demand that  $\delta h, \delta U, \delta W, \delta V$  enhancement parameters be equal to 0. It is possible, as  $U_1, V_1, W_1$  functions don't subject to any limitation and now we demand them to satisfy the equations mentioned above.

$$\begin{aligned}
 & \{r[B_{11} \frac{d}{dS} h \frac{dU_1}{dS} - \frac{B_{12}}{r} h \frac{dU_1}{dS} \sin \theta] + \frac{1}{R_1} [\frac{r}{12} [\frac{B_{11}}{R_1} \frac{d}{dS} h^3 \frac{dU_1}{dS} - \\
 & - \frac{B_{12}}{R_1} \frac{\sin \theta}{r} \frac{d}{dS} h^3 \frac{dU_1}{dS}]] + [B_{12} \frac{dhU_1}{dS} + B_{22} \frac{1}{r} hU_1 \sin \theta] \sin \theta + \\
 & + \frac{\sin \theta}{R_1} \frac{1}{12} [-\frac{B_{12}}{R_1} \frac{d}{dS} h^3 \frac{dU_1}{dS} + \frac{B_{22}}{R_1} \frac{\sin \theta}{r} h^3 U_{11}] + r \rho \omega^2 hU_1 + \quad (17)
 \end{aligned}$$

$$\begin{aligned}
 & [\frac{r}{12} (-\frac{B_{11}}{R_1} \frac{d^3}{dS^3} h^3 \frac{dW_1}{dS} - \frac{B_{12}}{R_1} \frac{\sin \theta}{r} \frac{d^2}{dS^2} h^3 W_1)] + \frac{\sin \theta}{12} \cdot \\
 & \cdot [\frac{B_{12}}{R_1} \frac{d^2}{dS^2} h^3 \frac{dW_1}{dS} - \frac{B_{22}}{R_1} \frac{\sin \theta}{r} \frac{d^2}{dS^2} h^3 W_1] - r \{ \frac{1}{R_1} [B_{12} \frac{d}{dS} h \frac{dW_1}{dS} + \\
 & + B_{12} \frac{1}{r} h \frac{dW_1}{dS} \sin \theta] + \frac{1}{R_2} [B_{12} \frac{d}{dS} h \frac{dW_1}{dS} + B_{22} \frac{1}{r} h \frac{dW_1}{dS} \sin \theta] \} = 0
 \end{aligned}$$

$$\begin{aligned}
 & \{r[-\frac{B_{11}}{R_1} h \frac{dU_1}{dS} + \frac{B_{12}}{r} h \frac{dU_1}{dS} \cos \theta] + \frac{1}{R_1} \{ \frac{r}{12} [-B_{11} \frac{d^2}{dS^2} \cdot \\
 & \cdot h^3 \frac{dU_1}{dS} + B_{12} \frac{\sin \theta}{r} \frac{d}{dS} h^3 \frac{dU_1}{dS} ] + [-\frac{B_{12}}{R_1} hU_1 - B_{22} \frac{1}{r} hU_1 \cdot \\
 & \cdot \cos \theta] \sin \theta + \frac{\sin \theta}{R_1} \frac{1}{12} [-B_{12} \frac{d^2}{dS^2} h^3 \frac{dU_1}{dS} + B_{22} \frac{\sin \theta}{r} h^3 \frac{dU_1}{dS} ] + \\
 & + [\frac{r}{12} (B_{11} \frac{d^3}{dS^3} h^3 \frac{dW_1}{dS} + B_{12} \frac{\sin \theta}{r} \frac{d^2}{dS^2} h^2 \frac{dW_1}{dS} )] + \frac{\sin \theta}{12} \cdot \quad (18) \\
 & \cdot [-B_{12} \frac{d^3}{dS^3} h^3 \frac{dW_1}{dS} + B_{22} \frac{\sin \theta}{r} \frac{d^2}{dS^2} h^3 \frac{dW_1}{dS} ] - r \{ [-\frac{B_{12}}{R_1} \cdot \\
 & \cdot h \frac{dW_1}{dS} - B_{12} \frac{1}{r} h \frac{dW_1}{dS} \cos \theta] + \frac{1}{R_2} [-\frac{B_{12}}{R_1} h \frac{\delta W_1}{dS} + B_{22} \frac{1}{r} h \frac{dW_1}{dS} \cdot \\
 & \cdot \cos \theta] \} + r \rho \omega^{-2} hW_1 = 0
 \end{aligned}$$

In this case  $\delta h$  factor must be 0, as  $\delta \bar{J} = 0$  at any  $\delta h$  case.

$$\begin{aligned}
 & \{r[-B_{11} \frac{dU_1}{dS} \frac{dU}{dS} - \frac{B_{11}}{R_1} \frac{dU_1}{dS} W - \frac{B_{12}}{r} \frac{dU_1}{dS} W \cos \theta - \frac{B_{12}}{r} \frac{dU_1}{dS} U \cdot \\
 & \sin \theta] + \frac{1}{R_1} \{ \frac{r}{12} [\frac{B_{11}}{R_1} h^2 \frac{d^2 W}{dS^2} \frac{dU_1}{dS} + \frac{3B_{11}}{R_1} \frac{d}{dS} h^2 \frac{dU_1}{dS} U - \\
 & - B_{12} \frac{\sin \theta}{r} \frac{d}{dS} 3h^2 \frac{dU_1}{dS} W - \frac{B_{12}}{R_1} \frac{\sin \theta}{r} \frac{d}{dS} 3h \frac{dU_1}{dS} U] \} + [-B_{12} \frac{dU}{dS} \cdot \\
 & U_1 - \frac{B_{12}}{R_1} WU_1 + B_{22} \frac{1}{r} WU_1 \cos \theta + B_{22} \frac{1}{r} UU_1 \sin \theta] \sin \theta + \frac{\sin \theta}{R_1} \frac{1}{12} \cdot \\
 & \cdot [3B_{12} h^2 \frac{d^2 W}{dS^2} \frac{dU_1}{dS} - \frac{3B_{12}}{R_1} \frac{d}{dS} h^2 \frac{dU_1}{dS} U - B_{22} \frac{\sin \theta}{r} 3h^2 \frac{dU_1}{dS} W + \\
 & + \frac{B_{22}}{R_1} \frac{\sin \theta}{r} 3h^2 UU_1] + r \rho \omega^2 UU_1 + [\frac{r}{12} (-B_{11} \frac{d^3}{dS^3} 3h^2 \frac{dW_1}{dS} \frac{dW}{dS} - \\
 & - \frac{B_{11}}{R_1} \frac{d^3}{dS^3} 3h^2 \frac{dW_1}{dS} U - B_{12} \frac{\sin \theta}{r} \frac{d^2}{dS^2} 3h^2 \frac{dW_1}{dS} \frac{dW}{dS} - \quad (19) \\
 & - B_{12} \frac{\sin \theta}{r} \frac{d^2}{dS^2} 3h^2 UW_1)] + \frac{\sin \theta}{12} [B_{12} \frac{d^2}{dS^2} 3h^2 \frac{dW_1}{dS} \frac{dW}{dS} + \\
 & + \frac{B_{12}}{R_1} \frac{d^2}{dS^2} 3h^2 \frac{dW_1}{dS} U - B_{22} \frac{\sin \theta}{r} \frac{d}{dS} 3h^2 \frac{dW_1}{dS} \frac{dW}{dS} - \frac{B_{22}}{R_1} \frac{\sin \theta}{r} \cdot \\
 & \cdot \frac{d^2}{dS^2} 3h^2 W_1 U] - r \{ \frac{1}{R_1} [-B_{12} \frac{dW_1}{dS} \frac{dU}{dS} - \frac{B_{12}}{R_1} \frac{dW_1}{dS} W + B_{12} \frac{1}{r} \frac{dW_1}{dS} \cdot \\
 & \cdot W \cos \theta + B_{12} \frac{1}{r} \frac{dW_1}{dS} U \sin \theta] + \frac{1}{R_2} [-B_{12} \frac{dW_1}{dS} \frac{dU}{dS} - \frac{B_{12}}{R_1} \frac{dW_1}{dS} W - \\
 & - B_{22} \frac{1}{r} \frac{dW_1}{dS} W \cos \theta + B_{22} \frac{1}{r} \frac{dW_1}{dS} U \sin \theta] \} + r \rho \omega^{-2} W W_1 = 0
 \end{aligned}$$

Based on (5), (7) and (18) systems similarity we have:  
 $U_1 = -UC, W_1 = WC$  (20)

If Equation (20) put on Equation (19) we will get:

$$\begin{aligned}
 & \{r[B_{11} \frac{d(UC)}{dS} \frac{dU}{dS} + \frac{B_{11}}{R_1} \frac{d(UC)}{dS} W + \frac{B_{12}}{r} \frac{d(UC)}{dS} W \cos \theta + \\
 & + \frac{B_{12}}{r} \frac{d(UC)}{dS} U \sin \theta] + \frac{1}{R_1} \{ \frac{r}{12} [-3B_{11} h^2 \frac{d^2 W}{dS^2} \frac{d(UC)}{dS} - \\
 & - \frac{3B_{11}}{R_1} \frac{d}{dS} h^2 \frac{d(UC)}{dS} U + B_{12} \frac{\sin \theta}{r} \frac{d}{dS} 3h^2 \frac{d(UC)}{dS} W + \\
 & + \frac{B_{12}}{R_1} \frac{\sin \theta}{r} \frac{d}{dS} 3h \frac{d(UC)}{dS} U] \} + [B_{12} \frac{dU}{dS} (UC) + \frac{B_{12}}{R_1} W (UC) - \\
 & - B_{22} \frac{1}{r} W (UC) \cos \theta - B_{22} \frac{1}{r} U (UC) \sin] \sin \theta + + \frac{\sin \theta}{R_1} \frac{1}{12} \cdot \\
 & \cdot [-3B_{12} h^2 \frac{d^2 W}{dS^2} \frac{d(UC)}{dS} + \frac{3B_{12}}{R_1} \frac{d}{dS} h^2 \frac{d(UC)}{dS} U + B_{22} \frac{\sin \theta}{r} \cdot \\
 & \cdot 3h^2 \frac{d(UC)}{dS} W - \frac{B_{22}}{R_1} \frac{\sin \theta}{r} 3h^2 U (UC)] - r \rho \omega^2 U (UC) + \quad (21) \\
 & + [\frac{r}{12} (-B_{11} \frac{d^3}{dS^3} 3h^2 \frac{d(WC)}{dS} \frac{dW}{dS} - \frac{B_{11}}{R_1} \frac{d^3}{dS^3} 3h^2 \frac{d(WC)}{dS} U -
 \end{aligned}$$

$$\begin{aligned}
 & -B_{12} \frac{\sin \theta}{r} \frac{d^2}{dS^2} 3h^2 \frac{d(WC)}{dS} \frac{dW}{dS} - B_{12} \frac{\sin \theta}{r} \frac{d^2}{dS^2} 3h^2 U(WC)] + \\
 & + \frac{\sin \theta}{12} [B_{12} \frac{d^2}{dS^2} 3h^2 \frac{d(WC)}{dS} \frac{dW}{dS} + \frac{B_{12}}{R_1} \frac{d^2}{dS^2} 3h^2 \frac{d(WC)}{dS} U - \\
 & - B_{22} \frac{\sin \theta}{r} \frac{d}{dS} 3h^2 \frac{d(WC)}{dS} \frac{dW}{dS} - \frac{B_{22}}{R_1} \frac{\sin \theta}{r} \frac{d^2}{dS^2} 3h^2 (WC)U] - \\
 & - r \{ \frac{1}{R_1} [-B_{12} \frac{d(WC)}{dS} \frac{dU}{dS} - \frac{B_{12}}{R_1} \frac{d(WC)}{dS} W + B_{12} \frac{1}{r} \frac{d(WC)}{dS} W \cdot \\
 & \cdot \cos \theta + B_{12} \frac{1}{r} \frac{d(WC)}{dS} U \sin \theta] + \frac{1}{R_2} [-B_{12} \frac{d(WC)}{dS} \frac{dU}{dS} - \\
 & - \frac{B_{12}}{R_1} \frac{d(WC)}{dS} W - B_{22} \frac{1}{r} \frac{d(WC)}{dS} W \cos \theta + B_{22} \frac{1}{r} \frac{d(WC)}{dS} U \cdot \\
 & \cdot \sin \theta] \} + r \rho \omega^2 W(WC) = 0
 \end{aligned}$$

#### IV. CONCLUSIONS

The Equation (21) with the Equation (5) to (7) system made close system  $U(\alpha)$ ,  $V(\alpha)$ ,  $W(\alpha)$ ,  $h(\alpha)$  for unknown functions. Solving this equations system, taking into consideration the appropriate (8) edge conditions, we will get the function of transformation of  $U$ ,  $V$ ,  $W$  and the function of describing the thickness of  $h$ .

$$\begin{aligned}
 & \frac{h^2}{4} \{ B_{11} [\frac{d}{dS} (\frac{dW}{dS} + \frac{U}{R_1})]^2 + 2B_{12} (\frac{dW}{dS} - \frac{U}{R_1}) \frac{d}{dS} (\frac{dW}{dS} - \frac{U}{R_1}) \frac{\sin \theta}{r} + \\
 & + B_{22} (\frac{dW}{dS} - \frac{U}{R_1})^2 \frac{\sin^2 \theta}{r^2} \} + B_{11} (\frac{dU}{dS} - \frac{U}{R_1})^2 + 2B_{12} (\frac{dU}{dS} + \frac{W}{R_1}) \cdot (22) \\
 & \cdot (\frac{W}{R_2} - \frac{U \sin \theta}{r}) + B_{22} (\frac{W}{R_2} - \frac{U \sin \theta}{r})^2 = \rho \omega^2 U^2 + \rho \omega^2 W^2
 \end{aligned}$$

Suggested technology has some advantages:

- It has an optimization system;
- It is cheaper;
- Getting a high qualitative production.

#### NOMENCLATURES

$\partial$ : Partial differentiation operator  
 $u, v, w$ : Displacements in the  $x, y,$  and  $z$  directions  
 $M$ : Weight of shell  
 $E$ : Young's modulus  
 $\Sigma$ : Summation  
 $D$ : Modulus of rigidity for isotropic material  
 $h$ : Shell thickness  
 $h_w(\alpha, \beta)$ : Changeable thickness  
 $dx$ : Differential distance in the  $x$  direction  
 $dy$ : Differential distance in the  $y$  direction  
 $dz$ : Differential distance in the  $z$  direction  
 $D_{ij}, (i,j=1,2,6)$ : Flexural rigidity matrix  
 $\alpha$ : Free fluctuation of shell  
 $v$ : Modulus of rigidity for isotropic material

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